

## HEAT TRANSFER

### ANALYSIS OF HEAT EXCHANGER

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#### The Effectiveness – NTU Method

This method is based on a dimensionless parameter called the heat transfer effectiveness,  $\varepsilon$ . Where

$$\varepsilon = \frac{q}{q_{\max}} = \frac{\text{actual heat transfer rate}}{\text{maximum possible heat transfer rate}}$$

The actual heat transfer rate can be determined from

$$q = C_c (T_{c,out} - T_{c,in})$$
$$q = C_h (T_{h,in} - T_{h,out})$$

Where

$$C_h = \dot{m}_h C_{ph}$$
$$C_c = \dot{m}_c C_{pc}$$

The maximum possible heat transfer rate is given by

$$q_{\max} = C_{\min} (T_{h,in} - T_{c,in})$$

Where  $C_{\min}$  is the smaller of  $C_h$  and  $C_c$  and  $\Delta T_{\max} = T_{h,in} - T_{c,in}$

The determination of  $q_{\max}$  requires the availability of the **inlet temperature** of the hot and cold fluids and their **mass flow rates**, which are usually specified. Then, once the effectiveness of the heat exchanger is known, the actual heat transfer rate  $q$  can be determined from

$$q = \varepsilon q_{\max}$$
$$q = \varepsilon C_{\min} (T_{h,in} - T_{c,in})$$

To determine the effectiveness,  $\varepsilon$  we involve a dimensionless quantity called **number of transfer units** which is expressed as

$$NTU = \frac{UA}{C_{\min}}$$

Take note how, the larger the NTU, the larger the heat exchanger.

Another dimensionless quantity used is the **capacity ratio**,  $c$  which is expressed as

$$c = \frac{C_{\min}}{C_{\max}}$$

Hence, the effectiveness of a heat exchanger which depends on the **geometry** of the heat exchanger as well as the **flow arrangement** can be determined from the expressions given in the table below.

**TABLE 13-4**

Effectiveness relations for heat exchangers:  $NTU = UA_s/C_{\min}$  and  $c = C_{\min}/C_{\max} = (\dot{m}C_p)_{\min}/(\dot{m}C_p)_{\max}$  (Kays and London, Ref. 5.)

Heat exchanger type	Effectiveness relation
1 <i>Double pipe:</i>	
Parallel-flow	$\varepsilon = \frac{1 - \exp[-NTU(1 + c)]}{1 + c}$
Counter-flow	$\varepsilon = \frac{1 - \exp[-NTU(1 - c)]}{1 - c \exp[-NTU(1 - c)]}$
2 <i>Shell and tube:</i>	
One-shell pass 2, 4, . . . tube passes	$\varepsilon = 2 \left\{ 1 + c + \sqrt{1 + c^2} \frac{1 + \exp[-NTU\sqrt{1 + c^2}]}{1 - \exp[-NTU\sqrt{1 + c^2}]} \right\}^{-1}$
3 <i>Cross-flow (single-pass)</i>	
Both fluids unmixed	$\varepsilon = 1 - \exp \left\{ \frac{NTU^{0.22}}{c} [\exp(-c NTU^{0.78}) - 1] \right\}$
$C_{\max}$ mixed, $C_{\min}$ unmixed	$\varepsilon = \frac{1}{c} (1 - \exp \{1 - c[1 - \exp(-NTU)]\})$
$C_{\min}$ mixed, $C_{\max}$ unmixed	$\varepsilon = 1 - \exp \left\{ -\frac{1}{c} [1 - \exp(-c NTU)] \right\}$
4 <i>All heat exchangers with <math>c = 0</math></i>	$\varepsilon = 1 - \exp(-NTU)$

The effectiveness,  $\varepsilon$  can also be determined graphically from Figure 13-26.

Subsequently, if we know  $\varepsilon$ , we can determine the NTU number from the expressions in the table below.

**TABLE 13–5**

NTU relations for heat exchangers  $NTU = UA_s/C_{\min}$  and  $c = C_{\min}/C_{\max} = (\dot{m}C_p)_{\min}/(\dot{m}C_p)_{\max}$  (Kays and London, Ref. 5.)

Heat exchanger type	NTU relation
1 <i>Double-pipe:</i> Parallel-flow	$NTU = -\frac{\ln [1 - \varepsilon(1 + c)]}{1 + c}$
Counter-flow	$NTU = \frac{1}{c - 1} \ln \left( \frac{\varepsilon - 1}{\varepsilon c - 1} \right)$
2 <i>Shell and tube:</i> One-shell pass 2, 4, . . . tube passes	$NTU = -\frac{1}{\sqrt{1 + c^2}} \ln \left( \frac{2/\varepsilon - 1 - c - \sqrt{1 + c^2}}{2/\varepsilon - 1 - c + \sqrt{1 + c^2}} \right)$
3 <i>Cross-flow (single-pass)</i> $C_{\max}$ mixed, $C_{\min}$ unmixed	$NTU = -\ln \left[ 1 + \frac{\ln (1 - \varepsilon c)}{c} \right]$
$C_{\min}$ mixed, $C_{\max}$ unmixed	$NTU = -\frac{\ln [c \ln (1 - \varepsilon) + 1]}{c}$
4 <i>All heat exchangers</i> with $c = 0$	$NTU = -\ln(1 - \varepsilon)$

### **Analysis of Heat Exchanger: Effectiveness – NTU Method**

1. A counter-flow double-pipe heat exchanger is to heat water from  $20^{\circ}\text{C}$  to  $80^{\circ}\text{C}$  at a rate of  $1.2\text{ kg/s}$ . The heating is to be accomplished by geothermal water available at  $160^{\circ}\text{C}$  at a mass flow rate of  $2\text{ kg/s}$ . The inner tube is thin-walled and has a diameter of  $1.5\text{ cm}$ . If the overall heat transfer coefficient of the heat exchanger is  $640\text{ W/m}^2 \cdot \text{K}$ , determine the length of the heat exchanger required to achieve the desired heating.
2. Hot oil is to be cooled by water in a 1-shell-pass and 8-tube-passes heat exchanger. The tubes are thin-walled and are made of copper with an internal diameter of  $1.4\text{ cm}$ . The length of each tube pass in the heat exchanger is  $5\text{ m}$ , and the overall heat transfer coefficient is  $310\text{ W/m}^2 \cdot ^{\circ}\text{C}$ . Water flows through the tubes at a rate of  $0.2\text{ kg/s}$ , and the oil through the shell at a rate of  $0.3\text{ kg/s}$ . The water and the oil enter at temperatures of  $20^{\circ}\text{C}$  and  $150^{\circ}\text{C}$ , respectively. Determine the rate of heat transfer in the heat exchanger and the outlet temperatures of the water and the oil.
3. Hot oil ( $C_p = 2200\text{ J/kg} \cdot \text{K}$ ) is to be cooled by water ( $C_p = 4180\text{ J/kg} \cdot \text{K}$ ) in a 2-shell-pass and 12-tube-pass heat exchanger. The tubes are thin-walled and are made of copper with a diameter of  $1.8\text{ cm}$ . The length of each tube pass in the heat exchanger is  $3\text{ m}$ , and the overall heat transfer coefficient is  $340\text{ W/m}^2 \cdot ^{\circ}\text{C}$ . Water flows through the tubes at a total rate of  $0.1\text{ kg/s}$ , and the oil through the shell at a rate of  $0.2\text{ kg/s}$ . The water and the oil enter at temperatures  $18^{\circ}\text{C}$  and  $160^{\circ}\text{C}$ , respectively. Determine the rate of heat transfer in the heat exchanger and the outlet temperatures of the water and the oil.